Effect of Normal, Beak and Tangential Grooves on Piston Crown of D.I. Diesel Engine with Blends of B10, B20 and B30 Apricot Bio-Diesel

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Abstract - Due to the rapid depletion of natural resources, which are ridiculously expensive for the common consumer, the value of petroleum fuels often rises, especially in India. Therefore, the importance of other fuel engines to be used in CI. Much researches were conducted on alternative fuels. Intensive research is being conducted within the area of improving the thermal efficiency of engines. This shows that in an exceedingly naturally aspirated internal-combustion engine, only one-third of the warmth supplied is converted to figure. Many methods are recommended by some experts and researchers to boost engine performance characteristics. the aim of this study is to extend the swirl effect within the cylinder, improve performance and reduce emissions. In DI diesel engines, vortices can increase the blending speed of fuel and air. The vortex interaction with the squish flow caused by compression increases the extent of turbulence within the combustion bowl and promotes mixing. it's clear that the effect of shape has little effect on the initial airflow during inspiratory and compression strokes. However, because the piston moves towards top spatial relation (TDC), the form of the bowl incorporates a significant effect on air flow, improving spraying, mixing and burning. In CI, the engine piston shape of the top was a flat and concave combustion chamber, and therefore the engine was powered by this shape. However, the air-fuel ratio mixture can't be mixed properly here. To avoid this, I changed the form of the piston.

Index Terms - D.I. Diesel Engine, Bio- Diesel, Apricot oil, Normal Piston, Beak Grooved Piston, Tangential Grooved Piston, B10, B20 and B30

INTRODUCTION

Energy is the most important aspect of economic and social development to improve quality of life. Most of the world's current energy sources are based on fossil fuels and will eventually run out unless we develop technologies that can use alternative fuels to supply energy [1]. Global energy consumption is increasing faster than population growth. Crude oil and petroleum products of this century are considered to be extremely rare and expensive. The daily fuel

consumption of the engine has improved and this will continue for years [2]. However, fuel demand is increasing rapidly due to the significant increase in the number of vehicles. Due to high energy consumption in developing countries, especially in Asia, this growth forecast is expected to increase by up to 1.5% by 2030.

Increasing energy demand has forced major fuel energy exporters around the world to find alternative fuels that are independent of fossil fuel-based products. Sustainability is a major issue leading to the fact that the energy sector is not fully developed, so various authorities are being called upon to use new renewable energy sources [3]. Biodiesel is one of the future success alternative fuels to solve this problem. Biodiesel is renewable, biodegradable, non-toxic and has properties very similar to diesel fuel. It can be made from both vegetable oils and animal fats. However, these oils can't be used directly as fuel due to high viscosity. In order to reduce viscosity, it is necessary to produce biodiesel to the transesterification process to remove glycerin from the product and ester [9]. Biodiesel can work with compressed ignition machinery, with or without modification as well as petroleum diesel. In addition, biodiesel is more effective in engine deductions, costs, and availability. If burned, biodiesel produces harmful contaminants for human health. In addition, it provides superior lubricants compared to diesel fuel. However, it is important to consider the performance and emission characteristics of the biodiesel fuel engine. In general, combustion of biodiesel fuel in a compression ignition (CI) engine produces less smoke, particulate matter, carbon monoxide, and hydrocarbons [8].

Objective of The Study:

The main purpose of this project is to study performance technologies to improve eddy in order to improve engine performance and reduce emissions in single-cylinder direct injection (DI) diesel engines. Changes have been made to the piston crown to achieve swirl strength in the cylinder. To increase the twist, a series of tests such as normal, beak and tangential grooves were performed on the piston crown and

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the results were compared to beak grooved and tangential grooved piston values and apricot as a biodiesel blend. The blend was obtained by blending diesel and esterified apricot kernel oil in the following ratios: B10 and D90 indicate that apricot biodiesel is 10% and diesel is 90%. Similarly, B20 & D80, B30 & D70 were made. Performance parameters such as braking efficiency, fuel consumption rate, and braking power have been determined.

Need of Alternative Fuels

Alternative fuels come from sources other than petroleum. Many of them are domestic and some come from renewable resources. The number of vehicles is increasing day by day, which means that fossil fuel consumption is also increasing exponentially. So far, we have relied on fossil fuels made from hydrocarbons that produce large amounts of non-renewable and harmful emissions. Alternative renewable fuels are urgently needed as hydrocarbon fuel reserves are rapidly depleted due to population explosions and technological improvements using higher fuel energy consumption. Organizations such as governments and environmental controls impose additional taxes and fines not only on automakers, but also on customers who violate car emission standards. To avoid all these problems, such alternatives to harmful emissions are needed and the fuel is essentially renewable.

Engine Specifications

ENGINE	FOUR STROKE SINGLE CYLINDER
ВНР	5 HP
SPEED	1500 RPM
FUEL	DIESEL
BORE DIA	80 MM
STROKE LENGTH	110 MM
METHOD OF COOLING	WATER COOLED
METHOD OF IGNITION	COMPRESSION IGNITION

EXPERIMENTAL SETUP



Figure 2.1 Image of Normal, Beak and Tangential Grooved Pistons Before Placing in to Cylinder

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Figure 2.2 Experimental Setup





Figure 2.3 Normal, Modified Beak and Tangential Grooved Pistons After Combustion

The piston crown of 80 mm diameter is modified by producing four grooves. In the present experiment, Beak Grooves of inner diameter 29.35 mm and outer 39.44 mm is produced on piston of 80 mm diameter and maintaining a depth of 1.5 mm at outer and 2 mm at inner in each groove for Beak Grooved

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Piston and Tangential Grooved with width of 8 mm and depth of 2 mm is produced on piston of 80 mm diameter and maintaining constant depth of 2 mm for Tangential Grooved Piston.

RESULTS AND DISCUSSIONS

The tests were carried by the modified Beak and Tangential grooved piston with a blend of B-10, B-20 & B-30 with a load

such as 2,4,6,8 and 10 kgs. Compared to Normal, Beak & Tangential grooved piston at full load of Bio-Diesel (B-20) reduction of brake specific fuel consumption in Beak, Tangential grooved piston is observed and at full load of Bio-Diesel (B-20) increase of brake thermal efficiency in Beak, Tangential grooved piston is observed.

S No	load(kg)	Engine speed in rpm	Time taken for 20cc of fuel in sec	Total mass of fuel consumption kg/hr	Brake power kW	Brake specific fuel consumption Kg/kWh	Brake mean effective pressure	Indicated power	Brake thermal efficiency	Indicated thermal efficiency	Mechanical efficiency
1	0	1500	136	0.4341	0	0	0	0	0	0	0
2	2	1500	136	0.4341	0.24	1.8087	555877.244	1.48	4.68	28.87	16.2162
3	4	1500	112	0.5271	0.74	0.7126	1713028.37	1.9796	11.88	31.81	37.3611
4	6	1500	96	0.615	1.233	0.4989	2855124.49	2.4727	16.97	34.05	49.8524
5	8	1500	88	0.6709	1.726	0.3887	3997220.61	2.9658	21.78	37.44	58.1900
6	10	1500	80	0.7268	2.219	0.2785	5139316.73	3.4589	26.59	40.83	66.5276

Table: 3.1 Normal Piston with only Diesel

S No	Applied load kg	Engine speed in rpm	Time taken for 20cc of fuel in sec	Total mass of fuel consumption kg/s	Brake power	Brake specific fuel consumption	Brake mean effective pressure	Indicated power	Brake thermal efficiency	Indicated thermal efficiency	Mechanical efficiency
1	0	1500	132	0.4472	0	0	0	0	0	0	0
2	2	1500	116	0.5089	0.24	2.12	555877.244	1.52	3.99	25.3	15.7895
3	4	1500	100	0.5904	0.74	0.7982	1713028.37	2.0196	10.61	28.97	36.6211
4	6	1500	92	0.6417	1.233	0.5205	2855124.49	2.5127	16.27	33.16	49.0588
5	8	1500	84	0.7768	1.726	0.4501	3997220.61	3.0058	18.81	32.77	57.4157
6	10	1500	76	0.9119	2.219	0.3797	5139316.73	3.4989	21.35	37.35	65.7726

Table: 3.2 Normal Piston with Apricot B-30%

S No	Applied load kg	Engine speed in rpm	Time taken for 20cc of fuel in sec	Total mass of fuel consumption kg/s	Brake power	Brake specific fuel consumption	Brake mean effective pressure	Indicated power	Brake thermal efficiency	Indicated thermal efficiency	Mechanical efficiency
1	0	1500	124	0.4761	0	0	0	0	0	0	0
2	2	1500	124	0.4761	0.24	1.9837	555877.244	1.39	4.26	24.73	17.2662
3	4	1500	104	0.5676	0.74	0.7674	1713028.37	1.8896	11.03	28.19	39.1406
4	6	1500	100	0.5904	1.233	0.4789	2855124.49	2.3827	17.68	34.18	51.7354
5	8	1500	92	0.6417	1.726	0.3718	3997220.61	2.8758	22.78	37.96	60.0111
6	10	1500	84	0.693	2.219	0.2647	5139316.73	3.3689	27.88	41.74	68.2868

Table: 3.3 Normal Piston With Apricot B-20%

S	Applied	Engine	Time	Total mass	Brake	Brake	Brake	Indicated	Brake	Indicated	Mechanical

No	load kg	speed in rpm	taken for 20cc of fuel in sec	of fuel consumption kg/s	power	specific fuel consumption	mean effective pressure	power	thermal efficiency	thermal efficiency	efficiency
1	0	1500	140	0.4217	0	0	0	0	0	0	0
2	2	1500	116	0.5089	0.24	2.1204	555877.244	1.5	3.99	24.96	16.0000
3	4	1500	104	0.5676	0.74	0.7674	1713028.37	1.9996	11.03	29.84	36.9874
4	6	1500	92	0.6417	1.233	0.5205	2855124.49	2.4927	16.27	32.9	49.4524
5	8	1500	76	0.7768	1.726	0.4501	3997220.61	2.9858	18.81	32.55	57.8003
6	10	1500	60	0.9119	2.219	0.3797	5139316.73	3.4789	21.35	35.96	66.1482

Table: 3.4 Normal Piston With Apricot B-10%

S No	Applied load kg	Engine speed in rpm	Time taken for 20cc of fuel in sec	Total mass of fuel consumption kg/hr	Brake power	Brake specific fuel consumption	Brake mean effective pressure	Indicated power	Brake thermal efficiency	Indicated thermal efficiency	Mechanical efficiency
1	0	1500	144	0.41	0	0	0	0	0	0	0
2	2	1500	160	0.3690	0.24	1.5375	555877.2438	1.04	5.5093	23.8737	23.0769
3	4	1500	128	0.4613	0.7396	0.6236	1713028.373	1.5396	13.5823	28.2739	48.0385
4	6	1500	112	0.5271	1.2327	0.4276	2855124.493	2.0327	19.8081	32.6632	60.6435
5	8	1500	108	0.5467	1.7258	0.3168	3997220.614	2.5258	26.7412	39.1372	68.3269
6	10	1500	104	0.5663	2.2189	0.206	5139316.73	3.0189	33.6743	45.6112	76.0103

Table:3.5 Beak Grooved Piston with Diesel

S No	Applied load kg	Engine speed in rpm	Time taken for 20cc of fuel in sec	Total mass of fuel consumption kg/s	Brake power	Brake specific fuel consumption	Brake mean effective pressure	Indicated power	Brake thermal efficiency	Indicated thermal efficiency	Mechanical efficiency
1	0	1500	148	0.3989	0	0	0	0	0	0	0
2	2	1500	148	0.3989	0.24	1.6622	555877.2438	1.52	5.0961	32.2755	15.7895
3	4	1500	116	0.5090	0.7396	0.6882	1713028.373	2.0196	12.3090	33.6117	36.6211
4	6	1500	104	0.5677	1.2327	0.4605	2855124.493	2.5127	18.3932	37.4922	49.0588
5	8	1500	100	0.5904	1.7258	0.3421	3997220.614	3.0058	24.7604	43.1248	57.4157
6	10	1500	96	0.6131	2.2189	0.2237	5139316.73	3.4989	31.1276	48.7574	65.7726

Table: 3.6 Beak Grooved Piston with Apricot B-30%

S No	Applied load kg	Engine speed in rpm	Time taken for 20cc of fuel in sec	Total mass of fuel consumption kg/s	Brake power	Brake specific fuel consumption	Brake mean effective pressure	Indicated power	Brake thermal efficiency	Indicated thermal efficiency	Mechanical efficiency
1	0	1500	144	0.41	0	0	0	0	0	0	0
2	2	1500	164	0.3600	0.24	1.5000	555877.2438	2.04	5.6471	48.0000	11.7647
3	4	1500	148	0.3989	0.7396	0.5394	1713028.373	2.5396	15.7046	53.9255	29.1227
4	6	1500	132	0.4473	1.2327	0.3628	2855124.493	3.0327	23.3453	57.4342	40.6469
5	8	1500	100	0.5904	1.7258	0.3421	3997220.614	3.5258	24.7604	50.5854	48.9478
6	10	1500	68	0.7335	2.2189	0.3214	5139316.73	4.0189	26.1755	60.9429	57.2487

Table: 3.7 Beak Grooved Piston with Apricot B-20%

S No	Applied load kg	Engine speed in rpm	Time taken for 20cc of fuel in sec	Total mass of fuel consumption kg/s	Brake power	Brake specific fuel consumption	Brake mean effective pressure	Indicated power	Brake thermal efficiency	Indicated thermal efficiency	Mechanical efficiency
1	0	1500	156	0.3785	0	0	0	0	0	0	0
2	2	1500	156	0.3785	0.24	1.5769	555877.2438	1.94	5.3716	43.4204	12.3711
3	4	1500	132	0.4473	0.7396	0.6047	1713028.373	2.4396	14.0068	46.2019	30.3164
4	6	1500	120	0.4920	1.2327	0.3991	2855124.493	2.9327	21.2230	50.4912	42.0329
5	8	1500	104	0.5677	1.7258	0.3289	3997220.614	3.4258	25.7508	51.1167	50.3766
6	10	1500	88	0.6434	2.2189	0.2587	5139316.73	3.9189	30.2786	51.7422	58.7203

Table: 3.8 Beak Grooved Piston with Apricot B-10%

S No	App lied load kg	Engin e speed in rpm	Time taken for 20cc of fuel in sec	Total mass of fuel consumpti on kg/hr	Brak e powe r	Brake specific fuel consumpti on	Brake mean effective pressure	Indicat ed power	Brake thermal efficien cy	Indicate d thermal efficien cy	Mechani cal efficienc y
1	0	1500	192	0.3075	0	0	0	0	0	0	0
2	2	1500	204	0.2894	0.24	1.2059	555877.2 438	2.54	7.0244	74.3415	9.4488
3	4	1500	188	0.3140	0.739 6	0.4246	1713028. 373	3.0396	19.9490	81.9863	24.3321
4	6	1500	176	0.3355	1.232 7	0.2721	2855124. 493	2.5327	31.1270	63.9534	48.6714
5	8	1500	168	0.3514	1.725 8	0.2036	3997220. 614	4.0258	41.5975	97.0351	42.8685
6	10	1500	160	0.3673	2.218	0.1351	5139316. 73	5.5189	52.068	130.116 8	73.0107

Table: 3.9 Tangential Grooved Piston with only Diesel

S No	App lied load kg	Engin e speed in rpm	Time taken for 20cc of fuel in sec	Total mass of fuel consumpti on kg/s	Brak e powe r	Brake specific fuel consumpti on	Brake mean effective pressure	Indicat ed power	Brake thermal efficien cy	Indicate d thermal efficien cy	Mechani cal efficienc y
1	0	1500	200	0.2952	0	0	0	0	0	0	0
2	2	1500	200	0.2952	0.24	1.2300	555877.2 438	2.64	6.8867	75.7532	9.0909
3	4	1500	200	0.2952	0.739 6	0.3991	1713028. 373	3.1396	21.2224	90.0890	23.5571
4	6	1500	176	0.3355	1.232 7	0.2721	2855124. 493	3.6327	31.1270	91.7296	33.9334
5	8	1500	160	0.3690	1.725	0.2138	3997220.	4.1258	39.6166	94.7099	41.8295

					8		614				
6	10	1500	144	0.4025	2.218 9	0.1555	5139316. 73	4.6189	48.1062	97.6902	49.7256

Table: 3.10 Tangential Grooved Piston with Apricot B-30%

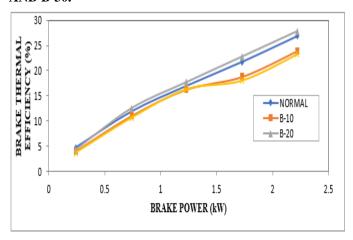
S No	App lied load kg	Engin e speed in rpm	Time taken for 20cc of fuel in sec	Total mass of fuel consumpti on kg/s	Brak e powe r	Brake specific fuel consumpti on	Brake mean effective pressure	Indicat ed power	Brake thermal efficien cy	Indicate d thermal efficien cy	Mechani cal efficienc y
1	0	1500	204	0.2894	0	0	0	0	0	0	0
2	2	1500	204	0.2894	0.24	1.2059	555877.2 438	3.24	7.0244	94.8293	7.4074
3	4	1500	188	0.3140	0.739 6	0.4246	1713028. 373	3.7396	19.9490	100.867 3	19.7775
4	6	1500	176	0.3355	1.232 7	0.2721	2855124. 493	4.2327	31.1270	106.880	29.1233
5	8	1500	164	0.3600	1.725 8	0.2086	3997220. 614	4.7258	40.6071	111.195 3	36.5187
6	10	1500	152	0.3845	2.218 9	0.1451	5139316. 73	5.2189	50.0872	112.893 1	43.9141

Table: 3.11 Tangential Grooved Piston with Apricot B-20%

S No	App lied load kg	Engin e speed in rpm	Time taken for 20cc of fuel in sec	Total mass of fuel consumpti on kg/s	Brak e powe r	Brake specific fuel consumpti on	Brake mean effective pressure	Indicat ed power	Brake thermal efficien cy	Indicate d thermal efficien cy	Mechani cal efficienc y
1	0	1500	196	0.3012	0	0	0	0	0	0	0
2	2	1500	192	0.3075	0.24	1.2813	555877.2 438	2.82	6.6112	77.6815	8.5106
3	4	1500	172	0.3433	0.739 6	0.4641	1713028. 373	3.3196	18.2512	81.9184	22.2798
4	6	1500	152	0.3884	1.232 7	0.3151	2855124. 493	3.8127	26.8824	83.1464	32.3314
5	8	1500	136	0.4341	1.725 8	0.2515	3997220. 614	4.3058	33.6741	84.0156	40.0808
6	10	1500	120	0.4798	2.218	0.1879	5139316. 73	4.7989	40.4658	84.8848	47.8302

Table: 3s.12 Tangential Grooved Piston with Apricot B-10%

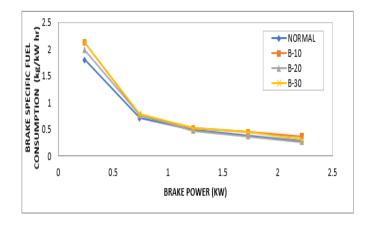
3.1 NORMAL PISTON WITH BLENDS OF B-10, B-20 AND B-30.



3.1.1 Brake thermal efficiency:

Fig- 3.1 Variation of Brake thermal efficiency with respect to Brake power at various blends

The brake thermal efficiency with brake power will conduct a performance test on normal piston with Diesel and Bio-Diesel blends. The brake thermal efficiency for the normal piston with full load is 26.59%. The brake thermal efficiency for the normal piston with B-10, B-20 and B-30 full load is 21.35%.27.88% and 21.35%. Comparison of normal piston and B-20 the brake thermal efficiency will increases up to 1.29%.



3.1.2 Brake specific fuel consumption:

Fig- 3.2 Variation of Brake specific fuel consumption with respect to Brake power at various blends

The brake specific fuel consumption with brake power is conducted with a performance test on normal piston and Diesel and Bio-Diesel blends. The brake specific fuel consumption for the normal piston with full load is 0.2785 kg/kW hr. The brake specific fuel consumption for the normal piston with B-10, B-20 and B-30 with full load is 0.3797 kg/kW hr, 0.2647 kg/kW hr and 0.3197 kg/kW hr. Comparison of normal piston and B-20 the brake specific fuel consumption is decreases up to 0.0138 kg/kW hr.

3.2 BEAK GROOVED PISTON WITH BLENDS B-10, B-20 AND B-30.

3.2.1 Brake thermal efficiency:

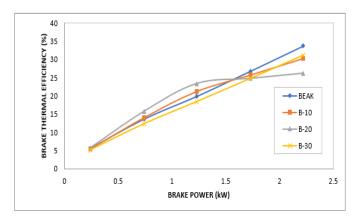
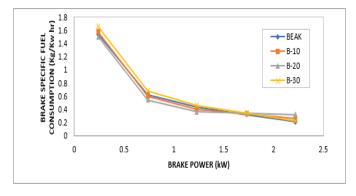


Fig- 3.1 Variation of Brake thermal efficiency with respect to Brake power at various blends

The brake thermal efficiency with brake power will conduct a performance test on beak grooved piston and Diesel and Bio-Diesel blends. The brake thermal efficiency for the beak grooved piston with full load is 33.67%. The brake thermal efficiency for the beak grooved piston with B-10, B-20 and B-30 with full load is 30.27%, 26.18% and 31.13%. Comparison of beak grooved piston and B-30 the brake thermal efficiency will decrease up to 2.54%.



3.2.2 Brake specific fuel consumption:

Fig- 3.2 Variation of Brake specific fuel consumption with respect to Brake power at various blends

The brake specific fuel consumption with brake power is conducted with a performance test on beak grooved piston and Diesel and Bio-Diesel blends. The brake specific fuel consumption for the beak grooved piston with full load is 0.206kg/kW hr. The brake specific fuel consumption for the beak grooved piston with B-10, B-20 and B-30 with full load is 0.2587 kg/kWhr,0.3214 kg/kW hr and 0.2237 kg/ kW hr. Comparison of beak grooved piston and B-20 the brake specific fuel consumption is increased up to 0.1154 kg/kW hr.

3.3 TANGENTIAL GROOVED PISTON WITH BLENDS B-10, B-20 AND B-30.

3.3.1 Brake thermal efficiency

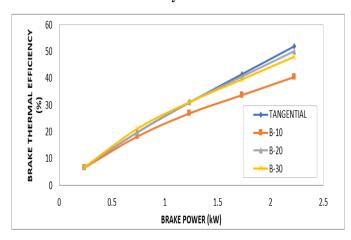


Fig- 3.6 Variation of Brake thermal efficiency with respect to Brake power at various blends

The brake thermal efficiency with brake power will conduct a performance test on tangential grooved piston and Diesel and Bio-Diesel blends. The brake thermal efficiency for the tangential piston with full load is 52.07%. The brake thermal efficiency for the tangential grooved piston with B-10, B-20 and B-30 with full load is 40.47%, 50.09% and 48.11%. Comparison of tangential grooved piston and B-30 the brake thermal efficiency will decrease up to 1.98%.

3.3.2 Brake specific fuel consumption:

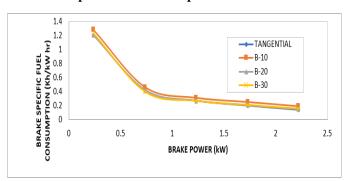


Fig- 3.7 Variation of Brake specific fuel consumption with respect to Brake power at various blends

The brake specific fuel consumption with brake power is conducted with a performance test on tangential grooved piston and Diesel and Bio-Diesel blends. The brake specific fuel consumption for the tangential grooved piston with full load is 0.1351kg/ kW hr. The brake specific fuel consumption for the tangential grooved piston withB-10, B-20 and B-30 with full load is 0.1879 kg/kWhr,0.1451 kg/kWhr and 0.1555 kg/ kW hr. Comparison of tangential grooved piston and B-20 the brake specific fuel consumption is increased up to 0.01 kg/ kW hr.

CONCLUSION

Based on the experimental results for the normal piston engine with tangential grooved piston configuration, the following conclusions are drawn:

- Compared to Normal & Beak grooved piston at full load of Bio-Diesel (B-30) the brake thermal efficiency in Beak grooved piston increased up to 1.29%.
- Compared to Normal & Beak grooved piston at full load of Bio-Diesel (B-20) the brake specific fuel consumption in Beak grooved piston is decreased up to 0.0567 kg/kW hr.
- Compared to normal & Tangential grooved piston at full load of Bio-Diesel (B-20) the brake thermal efficiency in Tangential grooved piston increased up to 22.20%.
- Compared to normal & Tangential grooved piston at full load of Bio-Diesel (B-20) the brake specific fuel consumption in Tangential grooved piston is decreased up to 0.1196 kg/kW hr.
- Compared to Tangential & Beak grooved piston at full load of Bio-Diesel (B-20) the brake thermal efficiency in Tangential grooved piston increased up to 23.91%.
- Compared to Tangential & Beak grooved piston at full load of Bio-Diesel (B-20) the brake specific fuel consumption in Tangential grooved piston is decreased up to 0.1763 kg/kW hr.

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